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#### TITLE OF THE INVENTION

FUEL ASSEMBLY AND THIMBLE SCREW OF THE SAME

#### CROSS-REFERENCE TO RELATED APPLICATIONS

5 This application is based upon and claims the  
benefit of priority from the prior Japanese Patent  
Applications No. 2001-107148, filed April 5, 2001,  
No. 2001-129035, filed April 26, 2001; and  
No. 2002-013333, filed January 22, 2002, the entire  
contents of all of which are incorporated herein by  
10 reference.

#### BACKGROUND OF THE INVENTION

##### 1. Field of the Invention

The present invention relates to a fuel assembly  
used in a nuclear reactor, and a thimble screw of the  
15 fuel assembly.

##### 2. Description of the Related Art

An example of a nuclear reactor currently widely  
used for power generation includes a pressurized water  
reactor (to be referred to as "PWR" hereinafter).  
20 A fuel assembly used by the PWR is generally a canless  
fuel assembly with no wrapper tube. The structure of  
the canless fuel assembly will be briefly described.  
Top and bottom nozzles each having a plurality of  
coolant flow holes are connected to each other with  
25 a plurality of control rod guide tubes extending  
parallel to each other.

More specifically, the upper ends of the control

rod guide tubes, i.e., so-called guide thimbles, are mechanically connected to the top nozzle, and the lower ends thereof are also mechanically connected to the bottom nozzle. These guide thimbles respectively  
5 accept the thin elongated control rods of a control rod cluster. Depending on the loading position of the fuel assembly in the core, the guide thimbles do not accept the control rods as they are not located at corresponding positions. In this case, the guide thimbles accept  
10 non fuel bearing components (NFBC) such as thimble plugs or burnable poisons. A plurality of grids are mounted on the guide thimbles. The fuel rods are accepted in the lattice openings and are elastically supported there.

15 Of the structure of the fuel assembly briefly described above, the structure of the connecting portion that connects the guide thimbles and bottom nozzle will be described in more detail with reference to the accompanying drawings.

20 FIG. 1 is an elevation schematically showing the structure of a fuel assembly applied to a PWR.

FIG. 2A is a sectional elevation showing part of the lower structure of this fuel assembly, and FIG. 2B is a bottom view of the same.

25 As shown in FIG. 1, a fuel assembly 1 has top and bottom nozzles 3 and 4 at upper and lower ends of elongated guide thimbles 2, and a top grid 5, middle

5 grids 6, and bottom grid 7 fixed to the guide thimbles 2 in the longitudinal direction. Each of the top and bottom grids 5 and 7 is formed from a large number of lattice frames using thin plates, and holds fuel rods 8.

The top nozzle 3 is a bottomed box-like structure with a substantially square horizontal section. The top nozzle 3 has a plurality of coolant flow holes and guide thimble mounting holes in its end plate corresponding to the bottom plate. In addition, a hold down spring 9 is attached to the upper portion of the top nozzle 3. The bottom nozzle 4 has a top or end plate with a substantially square shape when seen from above, where a plurality of coolant flow holes and guide thimble mounting holes are formed. Legs 10 are respectively integrally formed to project from the four corners of the lower surface of the end plate.

20 The top and bottom nozzles 3 and 4 are connected to the upper and lower ends of the plurality of hollow tube-like guide thimbles 2 by utilizing the mounting holes described above.

25 Referring to FIGS. 2A and 2B, the lower end of each hollow tube-like guide thimble 2 is welded to a thimble end plug 12, and is fixed to the bottom nozzle 4 with a thimble screw 14 through an insert 13. One top grid 5 and seven middle grids 6 are mounted on the guide thimbles 2 at intervals, and the bottom grid

7 is mounted on the guide thimbles 2 through its connecting structure. It should be understood that the number of middle grids 6 can be appropriately changed.

5 The bottom grid 7 is fixed to the upper portion of the insert 13. A drain hole 15 extends through the thimble screw 14 in the axial direction, and a rotation preventive pin 17 for preventing loosening of the thimble screw 14 is provided to a seat 16 of the drain hole 15. The drain hole 15 allows the coolant in use  
10 to flow in the core in a direction P shown in FIG. 2A.

Furthermore, the seat 16 has a spot facing hole 18 communicating with the lower portion of the drain hole 15 and reaching the bottom surface of the seat 16. The rotation preventive pin 17 does not interfere with  
15 the flow of the coolant flowing into the drain hole 15 in the direction P.

The fuel rods 8 are inserted in and supported by the aligned lattice openings of the upper, middle, and bottom grids 5, 6, and 7 one by one, thus forming  
20 the fuel assembly 1.

With this structure, the drain holes 15 of the thimble screws 14 guide the coolant into the guide thimbles 2 in the core, and the introduced coolant cools the non fuel bearing components mounted in the  
25 guide thimbles 2. The drain holes 15 also serve as holes for sending the inner coolant to the outside.

During a scram mode of the nuclear reactor,

the control rods are urgently inserted in the guide  
thimbles 2 by free fall. The drain holes 15 also serve  
as a restrictor for limiting the outflow velocity of  
the inner coolant so the fall impact is moderated. In  
5 other words, to assure the cooling function described  
above, the larger the diameter  $d$  of the drain hole 15  
of the thimble screw 14, the better. To moderate  
the fall impact produced when the control rods fall,  
the smaller the diameter  $d$ , the better, which is  
10 contradictory.

During the scram mode of the nuclear reactor, when  
the control rods are urgently inserted in the guide  
thimbles 2 by free fall, an excessively large impact  
occurs to the top nozzle 3. For this reason, the  
15 guide thimbles 2 respectively have thin tube-like  
dashpots 20. The dashpots 20 reduce the velocity of  
the control rods falling in the guide thimbles 2,  
thereby moderating the excessively large impact acting  
on the top nozzle 3.

20 According to an example of the fuel assembly 1  
with such dashpots 20, as shown in FIG. 3, a dashpot 20  
with a length of  $0.16L$  to  $0.18L$  is provided to the  
guide thimble 2 where  $L$  is the length of the guide  
thimble 2 along its axial direction. Therefore, the  
25 compression load acting on the guide thimble 2 in the  
axial direction may cause flexural deformation of the  
dashpot 20. In this case, the control rod may not be

inserted well.

For this reason, as shown in FIGS. 4 and 5,  
a technique is disclosed in which the length of  
the dashpot 20 of the guide thimble 2 is decreased.  
5 With this arrangement, the length of the dashpot 20  
with respect to the length L of the guide thimble 2 can  
be suppressed to fall within the range of  $0.03L$  to  
 $0.1L$ , so the flexural rigidity of the dashpot 20 is  
increased. This can prevent flexural deformation of  
10 the dashpot 20.

This guide thimble will be referred to as  
an improved guide thimble hereinafter. The lower  
structure of a fuel assembly 1 to which an improved  
guide thimble shown in FIG. 5 is applied is different  
15 from that of the fuel assembly 1 shown in FIG. 2A only  
in that sleeves 21 are provided at the bottom grids 7  
and that it has a dashpot 20 only at one portion, and  
is substantially the same as that of the fuel assembly  
shown in FIG. 2A.

20 In the fuel assembly to which the improved guide  
thimble is applied, the length of the dashpot 20 on the  
lower end side of the guide thimbles 2 is decreased, as  
shown in FIGS. 4 and 5. This increases the flexural  
rigidity of the dashpot 20 to prevent its flexural  
25 deformation. However, a so-called braking effect that  
moderates the fall velocity of the control rod is  
decreased.

In a PWR, its fall terminal velocity is limited from the viewpoint of ensuring the safety of the fuel assembly 1. Originally, the dashpot 20 is provided to the guide thimble 2 in an axial direction, as shown in FIG. 3, in order to moderate the fall velocity of the control rod such that the fall terminal velocity does not exceed a limit. For this reason, in the fuel assembly 1 employing the improved guide thimble as shown in FIGS. 4 and 5, a countermeasure that moderates the fall terminal velocity of the control rod must be provided by another means.

#### BRIEF SUMMARY OF THE INVENTION

The present invention has been made in view of the above situation, and has as its object to provide a fuel assembly in which an improved guide thimble is employed and the diameter of the drain hole of a thimble screw is adjusted so that a fall impact produced when a control rod falls is moderated, and flexural deformation of a dashpot is prevented, without impairing the cooling function of non fuel bearing components, and a thimble screw of the fuel assembly.

In order to achieve the above object, the present invention has the following means.

According to a first aspect of the present invention, there is provided a fuel assembly comprising a bottom nozzle set on a lower core plate of a nuclear reactor, a top nozzle with a hold down spring to urge

the bottom nozzle against the lower core plate,  
a plurality of control rod guide tubes which guide  
control rods, having passed through the top nozzle,  
toward the lower core plate, top, middle, and  
5 bottom grids mounted on the control rod guide tubes,  
a plurality of fuel rods held by the grids to be  
substantially parallel to the control rod guide tubes,  
a thin tube-like dashpot formed on each of the control  
rod guide tubes to reduce a fall velocity of a  
10 corresponding one of the control rods, a thimble screw  
which connects each of the control rod guide tubes to  
the bottom nozzle, and a drain hole formed to extend  
through the thimble screw. The dashpot has a large-  
diameter portion, at a lower portion thereof, with  
15 substantially the same diameter as that of each of the  
control rod guide tubes, and a diameter  $d$  of the drain  
hole falls within a range of  $0.04D < d < 0.08D$  where  $D$   
is an inner diameter of the large-diameter portion.

Hence, the coolant can be sufficiently supplied  
20 also from the viewpoint of assuring the cooling  
function of the non fuel bearing components. From the  
viewpoint of moderating the fall impact of the control  
rod as well, the terminal velocity of the control rod  
can be suppressed to be equal to or less than the fall  
25 velocity with which the fall impact of the control rod  
can be moderated. Therefore, flexural deformation of  
the dashpot can be prevented.



A fuel assembly according to a second aspect of the present invention has the following thimble screw.

More specifically, the thimble screw is disposed in a bottom nozzle so as to extend from a bottom  
5 surface side, has a drain hole extending in the thimble screw in a longitudinal direction from a spot facing hole of a seat to a distal end, is formed such that a coolant is supplied into the drain hole from the spot facing hole toward the distal end while the nuclear  
10 reactor operates and into the drain hole from a distal end side toward the spot facing hole during a scram mode, is locked to the bottom nozzle at the seat with a rotation preventive pin, and is provided with a coolant collision portion, at a drain hole side of the rotation  
15 preventive pin, against which the coolant flowing from the distal end side toward the spot facing hole collides in order to increase the pressure drop of the coolant during the scram mode.

Furthermore, a collision surface of this coolant  
20 collision portion against which the coolant collides forms a recessed surface ground in a V-shape from the distal end side toward the spot facing hole, a flat surface, or a recessed surface arcuately ground from the distal end side toward the spot facing hole.

25 With the above arrangement, the thimble screw can also serve as a diode. Thus, while the non fuel bearing components have the same cooling ability as

that of the conventional case, the decelerating effect of the control rod can be improved by the increase in fluid resistance.

5 A fuel assembly according to a third aspect of the present invention has the following thimble screw.

10 More specifically, the thimble screw is disposed in a bottom nozzle to extend from a bottom surface side, has first and second drain holes extending in the thimble screw in a longitudinal direction from a spot facing hole of a seat to a distal end, and is formed such that a coolant is supplied into the first and second drain holes from the spot facing hole toward a distal end side while the nuclear reactor operates and into the second and first drain holes from the distal end side toward the spot facing hole during a scram mode. The thimble screws is locked to the bottom nozzle at the seat with a rotation preventive pin. The first drain hole has an opening area smaller than an opening area of the spot facing hole and smaller than an opening area of the second drain hole at the distal end.

20 Furthermore, the thimble screw is provided with a coolant collision portion, at a first drain hole side of the rotation preventive pin, against which the coolant flowing from the distal end side toward the spot facing hole collides in order to increase the pressure drop of the coolant during the scram mode.

The collision surface of the coolant collision portion against which the coolant collides forms a recessed surface ground in a V-shape from the distal end side toward the spot facing hole, a flat surface, or a recessed surface arcuately ground from the distal end side toward the spot facing hole.

Since the thimble screw has the above arrangement, the coolant enters from the distal end side and is discharged in the form of a jet from the drain hole toward the rotation preventive pin. As the rotation preventive pin strongly functions as a fluid resistance, the pressure drop for the flow of the coolant in the scram mode can be increased, and the decelerating effect of the control rod can be improved. Meanwhile, the rotation preventive pin does not influence the flow rate resistance of the coolant when the nuclear reactor operates. Thus, the coolant flow rate is assured, and the cooling ability of the non fuel bearing components can maintain the same effect as that of the conventional case.

Additional objects and advantages of the invention will be set forth in the description which follows, and in part will be obvious from the description, or may be learned by practice of the invention. The objects and advantages of the invention may be realized and obtained by means of the instrumentalities and combinations particularly pointed out hereinafter.

# BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWING

The accompanying drawings, which are incorporated in and constitute a part of the specification, illustrate embodiments of the invention, and together with the general description given above and the detailed description of the embodiments given below, serve to explain the principles of the invention.

FIG. 1 is an elevation briefly showing the structure of a fuel assembly to be applied to a PWR;

FIG. 2A is a sectional elevation showing part of the lower structure of the fuel assembly to be applied to the PWR;

FIG. 2B is a bottom view of the fuel assembly to be applied to the PWR;

FIG. 3 is an elevation of a guide thimble with dashpots at two portions;

FIG. 4 is an elevation showing part of the lower structure of a fuel assembly to which an improved guide thimble is applied;

FIG. 5 is an elevation showing part of the lower structure of a fuel assembly to which an improved guide thimble is applied;

FIG. 6 is a graph showing the relationship between  $((\text{drain hole diameter } d \text{ of thimble screw})/(\text{inner diameter } D \text{ of lower large-diameter portion of guide thimble}))$  and  $((\text{fall terminal velocity } V \text{ of control rod})/(\text{limited fall terminal velocity } V_0 \text{ of$

control rod));

FIG. 7 is a graph showing the relationship between  
((drain hole diameter  $d$  of thimble screw)/(inner  
diameter  $D$  of lower large-diameter portion of guide  
thimble)) and ((coolant inflow amount  $C$  from thimble  
screw)/(coolant inflow amount  $C_0$  from thimble screw  
which is necessary for cooling non fuel bearing  
components));

FIG. 8 is a view showing a state wherein a  
rotation preventive pin for a thimble screw in a fuel  
assembly according to the second embodiment of the  
present invention is built into the thimble screw;

FIG. 9A is a view showing an example of the  
rotation preventive pin for the thimble screw in the  
fuel assembly according to the second embodiment of  
the present invention;

FIG. 9B is a view showing another example of  
the rotation preventive pin for the thimble screw in  
the fuel assembly according to the second embodiment of  
the present invention;

FIG. 9C is a view showing still another example of  
the rotation preventive pin for the thimble screw in  
the fuel assembly according to the second embodiment of  
the present invention;

FIG. 10 is a view showing an example of a thimble  
screw in a fuel assembly according to the third  
embodiment of the present invention; and

FIG. 11 is a view showing another example of a thimble screw in a fuel assembly according to the third embodiment of the present invention.

#### DETAILED DESCRIPTION OF THE INVENTION

5       The embodiments of the present invention will be described hereinafter with reference to the accompanying drawings.

      Regarding the reference numerals used to describe the following embodiments, the same reference numerals  
10       denote the same portions as those of FIGS. 1 to 5.

#### (First Embodiment)

      The first embodiment of the present invention will be described with reference to FIGS. 6 and 7.

      In a fuel assembly according the first embodiment  
15       of the present invention, the structure of a connecting portion for connecting its guide thimbles 2 and bottom nozzle 4 is as shown in FIGS. 2B and 4 or 5, and a so-called improved guide thimble is employed. An inner diameter D of the lower large-diameter portion of the  
20       guide thimble 2 and a diameter d of a drain hole 15 satisfy the following equation (1):

$$0.04D < d < 0.08D \quad \dots (1)$$

      The function of the fuel assembly according to this embodiment with the above arrangement will be  
25       described.

      FIG. 6 is a graph showing results obtained by measuring a terminal velocity V of a control rod

inserted in the guide thimble 2 by free fall in a fuel assembly 1 formed as shown in FIGS. 4 and 5, by using  $(d/D)$ , which is the ratio of the diameter  $d$  of the drain hole 15 of a thimble screw 14 to the inner diameter  $D$  of the lower large-diameter portion of the guide thimble 2, as a parameter.

The axis of ordinate indicates  $V/V_0$  obtained by dividing the terminal velocity  $V$  of the control rod inserted in the guide thimble 2 by free fall by a limited terminal velocity  $V_0$  determined from the viewpoint of moderating the fall impact of the control rod. More specifically, the range of  $(V/V_0) < 1$  is a range where the terminal velocity  $V$  of the control rod inserted in the guide thimble 2 by free fall can be suppressed to be lower than the limited terminal velocity  $V_0$ . The range of  $(V/V_0) \geq 1$  is a range where the terminal velocity  $V$  of the control rod inserted in the guide thimble 2 by free fall becomes equal to or more than the limited terminal velocity  $V_0$ .

As shown in FIG. 6, in the range of  $(d/D) < 0.08$ ,  $(V/V_0) < 1$  is established, and the terminal velocity  $V$  of the control rod inserted in the guide thimble 2 by free fall does not exceed the limited terminal velocity  $V_0$  but satisfies the design standard. In the range of  $(d/D) \geq 0.08$ ,  $(V/V_0) \geq 1$  is established, and the terminal velocity  $V$  of the control rod inserted in the guide thimble 2 by free fall exceeds the limited

terminal velocity  $V_0$  and does not satisfy the design standard.

Hence, from the viewpoint of the terminal velocity  $V$  of the control rod inserted in the guide thimble 2 by free fall, the diameter  $d$  of the drain hole 15 of the thimble screw 14 and the inner diameter  $D$  of the lower large-diameter portion of the guide thimble 2 must satisfy  $d < 0.08D$ .

As described earlier, the drain hole 15 of the thimble screw 14 serves to guide the coolant into the guide thimble 2 in order to cool the non fuel bearing components. From this viewpoint of assuring the cooling function, the larger the diameter  $d$  of the drain hole 15 of the thimble screw 14, the better.

FIG. 7 is a graph showing results obtained by measuring the cooling ability of the non fuel bearing components in a fuel assembly 1 formed as shown in FIGS. 4 and 5, by using  $(d/D)$ , which is the ratio of the diameter  $d$  of the drain hole 15 of a thimble screw 14 to the inner diameter  $D$  of the lower large-diameter portion of the guide thimble 2, as a parameter.

The axis of ordinate indicates  $C/C_0$  obtained by dividing a coolant inflow amount  $C$  from the thimble screw 14 by a coolant inflow amount  $C_0$  necessary for cooling the non fuel bearing components when  $(d/D)$  is used as the parameter. More specifically, in the range of  $(C/C_0) \leq 1$ , the coolant inflow amount  $C$  does not



exceed the necessary coolant inflow amount  $C_0$ . In the range of  $(C/C_0) > 1$ , the coolant inflow amount  $C$  exceeds the necessary coolant inflow amount  $C_0$ .

As shown in FIG. 7, in the range of  $(d/D) > 0.04$ ,  
5  $(C/C_0) > 1$  is established, and the coolant inflow amount  $C$  becomes larger than the necessary coolant inflow amount  $C_0$ . In the range of  $(d/D) \leq 0.04$ ,  $(C/C_0) \leq 1$  is established, and the coolant inflow amount  $C$  does not exceed the necessary coolant inflow  
10 amount  $C_0$ .

Hence, from the viewpoint of the cooling ability, the diameter  $d$  of the drain hole 15 of the thimble screw 14 and the inner diameter  $D$  of the lower large-diameter portion of the guide thimble 2 must satisfy  
15  $d > 0.04D$ .

In the fuel assembly according to this embodiment, an improved guide thimble is employed, and the inner diameter  $D$  of the lower large-diameter portion of the guide thimble 2 and the diameter  $d$  of the drain hole  
20 15 of the thimble screw 14 are adjusted to satisfy  $0.04D < d < 0.08D$ .

Hence, the coolant can be sufficiently supplied also from the viewpoint of assuring the cooling function of the non fuel bearing components. From the  
25 viewpoint of moderating the fall impact of the control rod as well, the terminal velocity  $V$  of the control rod can be suppressed to be equal to or less than the fall

velocity with which the fall impact of the control rod can be moderated. Therefore, flexural deformation of a dashpot 20 can be prevented.

(Second Embodiment)

5           The second embodiment of the present invention will be described with reference to FIG. 8 and FIGS. 9A to 9C.

FIG. 8 is a view showing a state wherein a rotation preventive pin 17 for a thimble screw 14 in  
10           a fuel assembly according to the present invention is built into the thimble screw 14.

FIGS. 9A, 9B, and 9C are views each showing a rotation preventive pin for a thimble screw in the fuel assembly according to this embodiment.

15           As shown in FIG. 8, a shaft 23 of the thimble screw 14 has a guide hole 24 as a hole extending from a spot facing hole 18 of a seat 16 to a drain hole 15 on the distal end side in the longitudinal direction of the thimble screw 14. With the rotation preventive pin  
20           17 being mounted in the spot facing hole 18, during operation of the nuclear reactor, a coolant enters from the spot facing hole 18 of the seat 16 as shown in the direction indicated by an arrow A and is drained from a drain hole distal end 25. If the control rod is  
25           dropped in the scram mode, the coolant enters the drain hole 15 from the drain hole distal end 25 as shown in the direction of an arrow F and is drained from the

spot facing hole 18 of the seat 16.

In the thimble screw 14 of the fuel assembly according to this embodiment, the rotation preventive pin 17 has, at its upper side namely the guide hole 24 side, a water receiving machined portion 26 formed of a recess with an arcuate section, so it receives the flow of the coolant passing through the guide hole 24 in the direction indicated by the arrow F in FIG. 8. The water receiving machined portion 26 increases the pressure drop of the coolant flowing in the direction of the arrow F.

FIGS. 8 and 9C show an arcuate machined portion 30 formed of a recess with an arcuate section as a typical example of the rotation preventive pin 17 with the water receiving machined portion 26. Alternatively, the water receiving machined portion 26 may be a V-shaped machined portion 28 with a V-shaped section, as shown in FIG. 9A, or a flat machined portion 29, as shown in FIG. 9B. The water receiving machined portion 26 can have any shape as far as it can increase the pressure drop in the direction of the arrow F against the flow of the coolant passing through the guide hole 24 in the direction of the arrow F, when compared to a conventional case wherein a rotation preventive pin without a water receiving machined portion 26 is used.

With the structure of the conventional rotation preventive pin, the ratio of the pressure drop

coefficient for the flow of the coolant entering from the spot facing hole 18 of the seat 16 and draining from the drain hole distal end 25 as shown in the direction of the arrow A, to the pressure drop coefficient of the flow of the coolant entering from the drain hole distal end 25 and draining from the spot facing hole 18 of the seat 16 as shown in the direction of the arrow F, in the opposite manner, is almost 1 : 1.

10           The thimble screw 14 of the fuel assembly according to this embodiment has the rotation preventive pin 17 with the above arrangement. Thus, the ratio of the pressure drop coefficient of the flow of the coolant entering from the spot facing hole 18 of the seat 16 and draining from the drain hole distal end 25 as shown in the direction of the arrow A, to the pressure drop coefficient of the flow of the coolant entering from the drain hole distal end 25 and draining from the spot facing hole 18 of the seat 16 as shown in the direction of the arrow F, in the opposite manner, can be raised to the range of 1 : 2 to 1 : 3.

25           With the thimble screw 14 of the fuel assembly according to this embodiment, when the rotation preventive pin 17 with the shape as described above is used, the thimble screw 14 can also serve as a diode. Thus, while the non fuel bearing components have the same cooling ability as that of the conventional case,

which is caused by the flow of the coolant in the direction of the arrow A, the decelerating effect of the control rod can be improved by the increase in fluid resistance against the flow in the direction of the arrow F.

(Third Embodiment)

The third embodiment of the present invention will be described with reference to FIGS. 10 and 11.

FIGS. 10 and 11 are views each showing a thimble screw in a fuel assembly according to this embodiment.

In a thimble screw 14 for the fuel assembly according to this embodiment, a guide hole 24 is formed in the thimble screw 14 on a distal end side 31, and a drain hole 15 is arranged in the thimble screw 14 on a seat 16 side.

Referring to FIG. 10, a shaft 23 of the thimble screw 14 has the drain hole 15 extending between the guide hole 24 and a spot facing hole 18 of the seat 16. The opening area of the drain hole 15 is set smaller than the opening area of the guide hole 24 or the opening area of the spot facing hole 18. With a rotation preventive pin 17 being mounted in the spot facing hole 18, during operation of the nuclear reactor, a coolant enters from the spot facing hole 18 of the seat 16 in the direction of an arrow A in FIG. 10 and is drained from a guide hole distal end 32.

When a control rod is dropped in the scram mode,

the coolant flows in the direction of an arrow F and enters from the guide hole distal end 32 to flow through the spot facing hole 18 of the seat 16.

After passing through the drain hole 15, the coolant  
5 forms a jet as the flow path area is abruptly increased by the spot facing hole 18 of the seat 16, and jets out toward the rotation preventive pin 17.

With this arrangement, when the control rod is dropped in the scram mode and the coolant enters from  
10 the distal end side 31 in the direction of the arrow F, the rotation preventive pin 17 functions strongly as the fluid resistance against the jet. Thus, the pressure drop against the flow of the coolant in the direction of the arrow F can be increased, and the  
15 decelerating effect of the control rod can be improved.

In the thimble screw 14 of the fuel assembly shown in FIG. 11, the rotation preventive pin 17 with the water receiving machined portion 26 in the thimble screw 14 shown in FIG. 8 and FIG. 9A, 9B, or 9C is  
20 combined with the thimble screw 14 with the arrangement shown in FIG. 10. This rotation preventive pin 17 has a water receiving machined portion 26, in the same manner as the rotation preventive pin 17 of the second embodiment.

25 Since the thimble screw of the fuel assembly according to this embodiment has the above arrangement, the coolant enters from the guide hole distal end 32 in

the direction of the arrow F shown in FIG. 10 and is discharged in the form of a jet from the drain hole 15 toward the rotation preventive pin 17. As the rotation preventive pin 17 strongly functions as a fluid resistance against the jet, the pressure drop for the flow of the coolant in the direction of the arrow F can be increased, and the decelerating effect of the control rod can be improved. Meanwhile, the rotation preventive pin 17 does not influence the flow rate resistance of the coolant in the direction of the arrow A. Thus, the coolant flow rate is assured, and the cooling ability of the non fuel bearing components can maintain the same effect as that of the conventional case.

When the rotation preventive pin 17 with the water receiving machined portion 26 is combined with a thimble screw in which the opening area of the drain hole 15 is set smaller than the opening area of the guide hole 24 or the opening area of the spot facing hole 18, as in the thimble screw 14 of the fuel assembly shown in FIG. 11, the difference in pressure drop of the flow in the direction of the arrow A or F further increases. Therefore, a thimble screw for a fuel assembly with a better diode performance can be provided.

Additional advantages and modifications will readily occur to those skilled in the art. Therefore,

the invention in its broader aspects is not limited to the specific details and representative embodiments shown and described herein. Accordingly, various modifications may be made without departing from the spirit or scope of the general inventive concept as  
5 defined by the appended claims and their equivalents.